

# Reliability-based sensitivity analysis under distribution parameter uncertainty

## – Application to aerospace systems

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### Context & Motivations

- Evaluate the performances of complex aerospace systems
- Models, codes, variables rely on multiple sources of information affected by uncertainties (aleatory and epistemic)

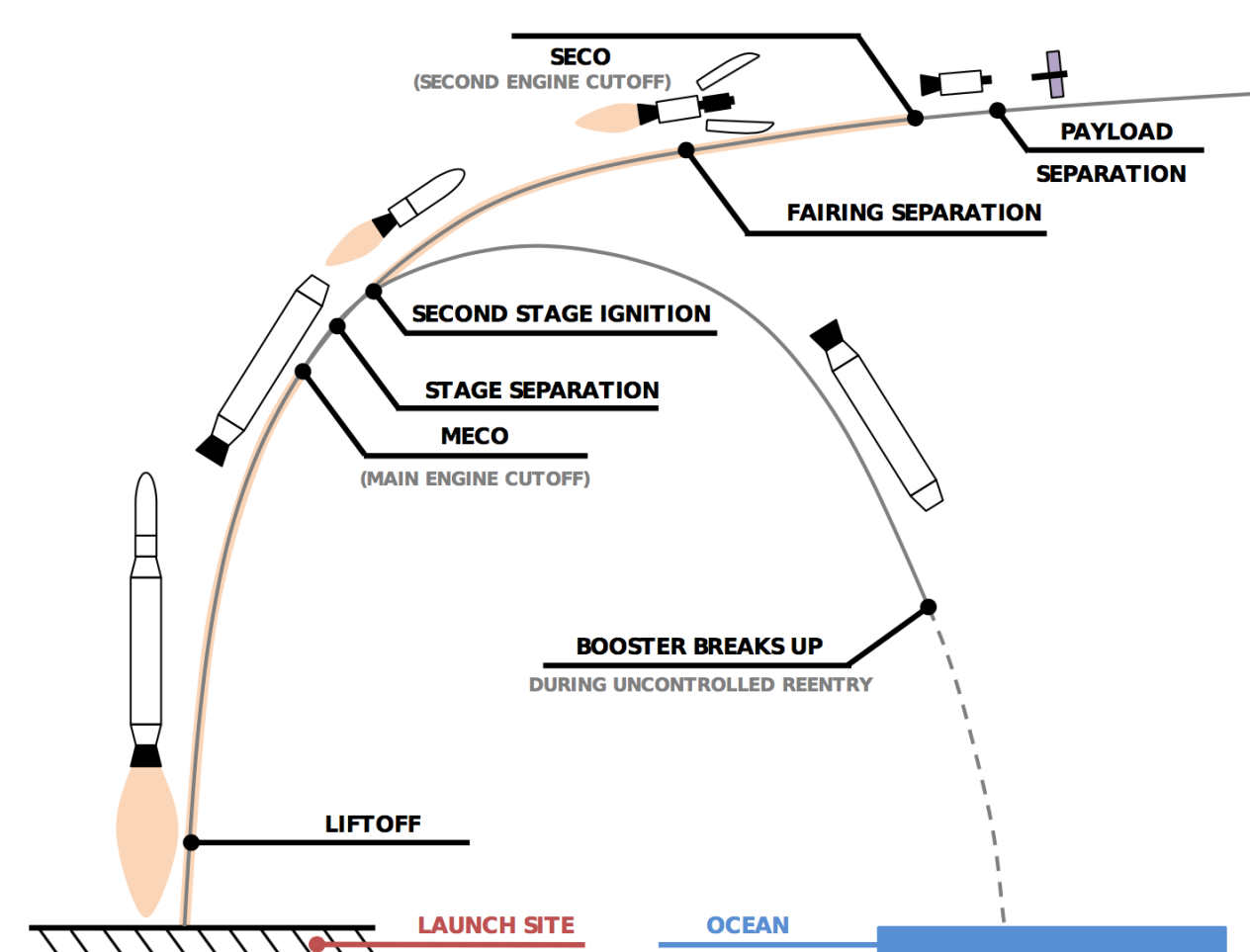


Figure: Launch vehicle fallback zone estimation.

### Notations & Problem statement

- Expensive-to-evaluate deterministic & static computer code  $\Leftrightarrow$  **black box model**

$$\mathcal{M} : \mathbb{R}^d \rightarrow \mathbb{R}, \mathbf{X} \mapsto Y = \mathcal{M}(\mathbf{X}) \quad (1)$$

- Limit-state function  $\Leftrightarrow$  **failure/safety of the system**

$$g : \mathbb{R}^d \rightarrow \mathbb{R}, \mathbf{X} \mapsto g(\mathbf{X}) = y_{th} - Y \quad (2)$$

- Hierarchical model in input:

- (level 1 - stochastic)  $\mathbf{X} \sim f_{\mathbf{X}|\Theta}(\mathbf{x}|\theta) : \mathcal{D}_{\mathbf{X}} \subseteq \mathbb{R}^d \rightarrow \mathbb{R}_+$
- (level 2 - stochastic)  $\Theta \sim f_{\Theta|\xi}(\theta|\xi) : \mathcal{D}_{\Theta} \subseteq \mathbb{R}^k \rightarrow \mathbb{R}_+$
- (level 3 - deterministic)  $\xi = (\xi_1, \xi_2, \dots, \xi_q)^T \in \mathcal{D}_{\xi} \subseteq \mathbb{R}^q$

### Issues

How to deal with this **bi-level uncertainty**?

- 1 Choose an a priori model for the uncertainty affecting  $\Theta$  (**modeling**)
- 2 Propagate the bi-level uncertainty in the failure probability estimation (**propagation**)
- 3 Link the variability of the failure probability to the input uncertainty (**sensitivity**)

### Uncertainty propagation via the Augmented Reliability Approach

- Conditional failure probability:

$$P_f(\theta) = \mathbb{P}[g(\mathbf{X}) \leq 0 | \theta = \theta] = \int_{\mathcal{D}_{\mathbf{X}}} \mathbb{1}_{\mathcal{F}_x}(\mathbf{x}) f_{\mathbf{X}|\theta}(\mathbf{x}|\theta) d\mathbf{x} \quad (3a)$$

- Predictive failure probability (PFP) [1]:

$$\tilde{P}_f(\xi) = \int_{\mathcal{D}_{\Theta}} \int_{\mathcal{D}_{\mathbf{X}}} \mathbb{1}_{\mathcal{F}_x}(\mathbf{x}) f_{\mathbf{X}|\theta}(\mathbf{x}|\theta) f_{\Theta|\xi}(\theta|\xi) d\mathbf{x} d\theta \quad (4a)$$

$$= \int_{\mathcal{D}_{\mathbf{Z}}} \mathbb{1}_{\mathcal{F}_z}(\mathbf{z}) f_{\mathbf{Z}|\xi}(\mathbf{z}|\xi) d\mathbf{z} \quad (4b)$$

- Nested (NRA) vs. **Augmented Reliability Approach (ARA)**

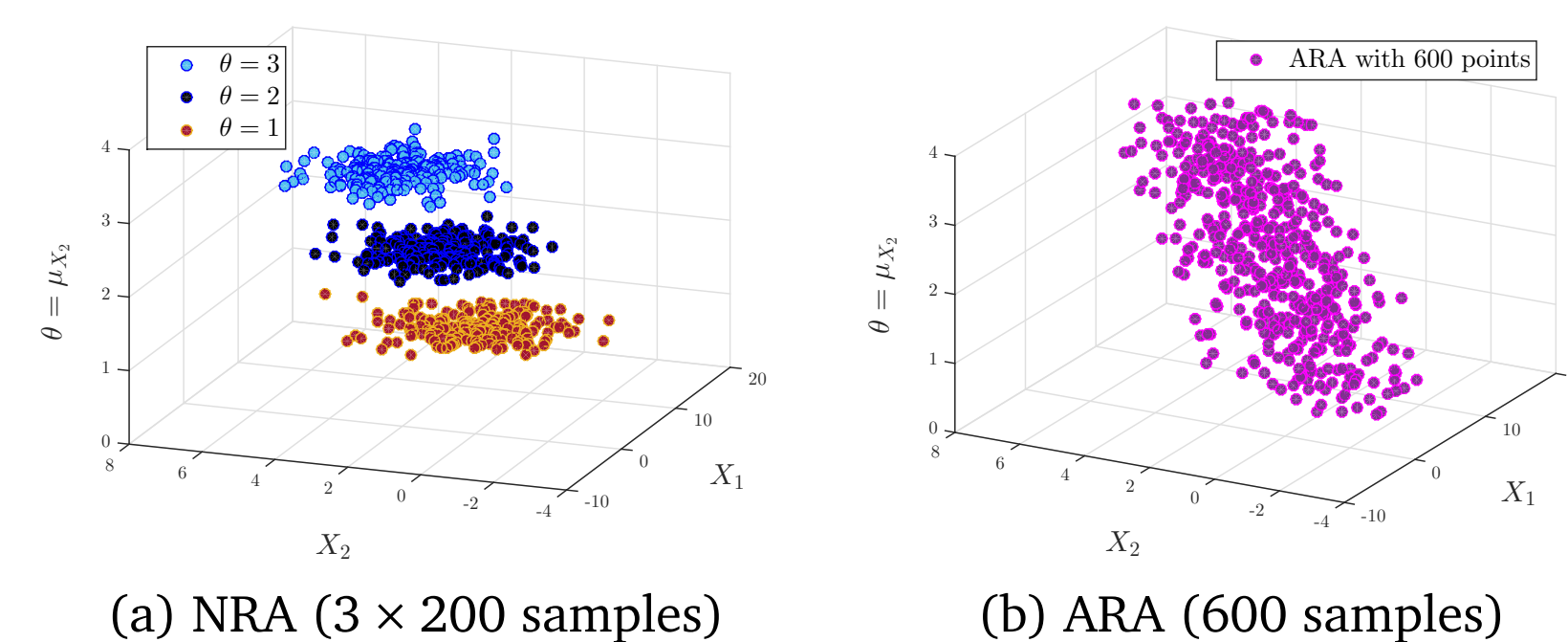


Figure: NRA vs. ARA for  $X_1 \sim \mathcal{N}(7, 5/\sqrt{3})$ ,  $X_2 \sim \mathcal{N}(\theta, 2/\sqrt{3})$  and  $\theta \sim \mathcal{N}(2, 1.5)$ .

$\hookrightarrow$  V. Chabridon et al. "Evaluation of failure probability under parameter epistemic uncertainty: application to aerospace system reliability assessment". *Aerospace Science and Technology* 69 (2017) 526-537.

$\hookrightarrow$  V. Chabridon et al. "Some Bayesian insights for statistical tolerance analysis". *23<sup>ème</sup> Congrès Français de Mécanique (CFM 2017)*, Lille.

### Local reliability-based sensitivity analysis

- Derivations of local sensitivity estimators of the PFP w.r.t. deterministic hyper-parameters:

- 1 Unbounded distribution for  $\Theta$ :

$$S_j \stackrel{\text{def}}{=} \frac{\partial \tilde{P}_f(\xi)}{\partial \xi_j} \approx \frac{1}{\text{MC}} \sum_{i=1}^N \mathbb{1}_{\mathcal{F}_z}(\mathbf{z}^{(i)}) \kappa_j(\theta^{(i)}, \xi) \quad (5)$$

- 2 Bounded distribution [2] for  $\Theta$ :

$$S_j \propto f_{X_j|\theta_j}(x_j|\theta_j = u/l\text{-bound}) \left( \tilde{P}_f - p_{f,\text{aux}}^{\theta_j = u/l\text{-bound}} \right) \quad (6)$$

- Estimation strategy: augmented Nonparametric Adaptive Importance Sampling (NAIS)

$\hookrightarrow$  V. Chabridon et al. "Reliability-based sensitivity analysis of aerospace systems under distribution parameter uncertainty using an augmented approach". *ICOSSAR 2017*, Vienna.

$\hookrightarrow$  V. Chabridon et al. "Reliability-based sensitivity estimators of rare event probability under distribution parameter uncertainty". (Under Review) *Reliability Engineering & System Safety*.

### Conclusions

- $\tilde{P}_f(\xi)$  can be a relevant measure of safety for design purposes (but may not be sufficient for risk management)
- Robustness of this measure w.r.t. some priori choices is investigated in terms of sensitivity analysis
- Local and global sensitivities can be obtained by efficient numerical sampling compared to CMC

### Perspectives

- To use metamodels to speed up the calculations or to get the sensitivity measures as by-products of the metamodeling step

### References

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